

Ventilation during Anesthesia: From Automatic Human Hand to Intelligent Machine!

INTRODUCTION

Manual ventilation during anesthesia and surgery, particularly in the prolonged procedures, is tiring to an anesthesiologist and adds an element of danger to a patient. In spite of advances in locoregional anesthesia and its widespread usage, general anesthesia with mechanical ventilation still holds the center stage in the intraoperative management of many surgical procedures. Less than a quarter-century ago, induction of anesthesia was mostly followed by paralysis using succinylcholine and endotracheal intubation. After recovery from succinylcholine, the patients were allowed to breathe spontaneously. If continued muscle relaxation was required, mechanical ventilation was manual with no monitoring whatsoever. An anesthetist was most often blissfully unaware of any changes. Needless to say, that the variations would be more with a tired and sleepy anesthetist at the head-end of the patient. Gone are those days of mechanical ventilation being heavily dependent on the “acquired automaticity” of the anesthetist’s hands!

The venture of artificial ventilators into anesthesia practice began when surgeons started performing more extensive thoracic surgeries. A major boost to the development of automatic artificial ventilators occurred in 1952 when there was a polio epidemic in Denmark. They were primarily body enclosing devices^[1] and iron lung devices.^[2,3] These early devices were based on the principle of *negative pressure ventilation*. The limitations of usage of these mega-size ventilators together with a better understanding of the lung mechanics and physiology led to the development of *positive pressure ventilation*. By the first half of 20th century, the focus of ventilators shifted from just providing ventilator support to the patient to treating oxygenation failure. The concept of positive pressure ventilation took a major leap with subsequent identification of acute respiratory distress syndrome (ARDS).^[4]

MODES OF VENTILATION

In the 1950s and 1960s, there were only two modes of ventilation used either in intensive care units (ICUs) or in operating room. They were *pressure-limited ventilation* and *volume-regulated ventilation*. All modes of mechanical ventilation were derived from one or a combination of these two base systems. In the initial days, ventilators were primarily volume-controlled modes because they delivered a preset tidal volume (V_T) independently from the patient’s lung mechanics.^[5] Conventionally, moderately high V_T (10–12 mL/kg), low respiratory rates (8–10 breaths/min), inspiration to expiration ratio (1:2), slightly increased fraction

of inspired oxygen (F_{iO_2}) (30%–50%), and zero end-expiratory pressure were used.

The concept of intermittent mandatory ventilation was introduced in the 1970s to assist in weaning patients from ventilators which were later modified to allow for better synchronization and to prevent breath stacking. In the last few decades, the technical aspects of ventilators have dramatically improved with respect to better flow delivery, use of microprocessors, improved triggering, and development of newer modes of mechanical ventilation. Moreover, all these are available in the ventilators integrated into the anesthesia machine. Toward the end of surgery, when the patients are recovering from the effect of muscle relaxant, they are often ventilated with synchronized intermittent mandatory ventilation mode. Similarly, when a supraglottic airway is being used to provide anesthesia, pressure support mode or synchronized intermittent mandatory ventilation mode is used to augment the patient’s spontaneous ventilation.

There is greater flexibility and safety in the ventilation of even critically ill patients undergoing surgery. Modes such as inverse ratio ventilation and dual modes such as pressure control with volume guarantee are now available on anesthesia ventilators. High-frequency jet ventilation used intraoperatively, e.g., during video-assisted thoracoscopic surgery, represents extension of critical care to the operating theater whereas surgeries performed on patients while on extracorporeal membrane oxygenation represents exactly the reverse.

RESPIRATORY MONITORING

Monitoring of ventilation was mainly clinical three decades ago where the chest expansion, auscultation of breath sounds, and color of the lips, nail bed, and the surgical field were all that was possible to monitor. Present-day monitoring of respiration includes pulse oximetry, capnography, airway pressures, and ventilator graphics (flow-time, pressure-time, and volume-time scalars as well as the flow-volume and pressure-volume loops) complemented with arterial blood gas analysis as required.

Ventilator-induced lung injury

Intraoperative mechanical ventilation is typically focused on maintaining homeostasis. As the old adage goes, “First of all, do no harm,” preventing injury to the surgical patient under anesthesia is equally important. One of the major concerns of mechanical ventilation is the development of ventilator-induced lung injury (VILI), which is caused by volutrauma and barotrauma resulting in an enhanced systemic inflammatory response with worsening oxygenation. VILI was

identified in patients with acute lung injury (ALI) requiring mechanical ventilation. Subsequently, the possibility of it developing in patients undergoing routine general endotracheal anesthesia was studied. As an extension to the ARDS net study,^[6,7] Choi *et al.* compared the use of V_T of 12 mL/kg without positive end-expiratory pressure (PEEP) with V_T of 6 mL/kg with PEEP of 10 cm H₂O in patients undergoing major abdominal surgery. They found that the usage of large V_T without PEEP caused systemic inflammation and lung injury in patients with no lung disease.^[8] It is now clear that the principles of intraoperative mechanical ventilation should be similar to that in the ICU setting because of the difficulty in diagnosing ALI/ARDS and the potential for multiple hits caused by intraoperative volutrauma.^[9]

Postoperative pulmonary complications (PPCs) are known to be associated with longer hospital stays and higher long-term mortality rates.^[10] Certain intraoperative protective mechanical ventilation strategies have been defined to minimize the occurrence of VILI such as the rational use of the FiO_2 , V_T and PEEP.^[11] The latest parameter that is being evaluated is the driving pressure.

Fraction of inspired oxygen

Indiscriminate use of high FiO_2 and its association with direct pulmonary toxicity, interstitial fibrosis, reabsorption atelectasis, and tracheobronchitis is well documented.^[12] Hence, it is recommended that the lowest possible FiO_2 is used to prevent hypoxia and to avoid hyperoxia. Although there is no robust evidence to recommend an ideal FiO_2 in surgical patients, a minimum possible FiO_2 to maintain a peripheral arterial saturation (SpO_2) level above 92% is recommended in nonobese surgical patients with healthy lungs undergoing open abdominal surgery.^[12]

Tidal volume

Historically, high V_T values (up to 15 mL/kg predicted body weight [PBW]) were used intraoperatively to increase the end-expiratory lung volume and to reduce the incidence of atelectasis.^[13] In later years, it was found that usage of low V_T values was associated with a reduction in lung injuries induced by mechanical ventilation and has been consistently recommended for pulmonary protection during the intraoperative period.^[14] Large randomized clinical trials have demonstrated that intraoperative ventilation with a V_T of 6–8 mL/kg PBW prevents the development of PPC in patients undergoing elective surgery.^[15,16]

Positive end-expiratory pressure

Current evidence shows that the use of PEEP can reduce atelectasis, improve compliance without increasing dead space, and maintain the end-expiratory volume in obese and nonobese patients under general anesthesia.^[10]

Driving pressure

The stretch of lung produced by mechanical ventilation can produce stress and strain of the alveoli and consequent lung injury.^[17,18] The total increase in transpulmonary pressure due to

the V_T and PEEP represents the stress imposed on the lung. The distension obtained or the deformation of the lung (increase in lung volume above the resting volume) in response represents the strain on the lung. The volume increase due to PEEP can be termed static (as it is constant pressure throughout respiratory cycle) whereas that due to the V_T is termed dynamic (as it changes during the respiratory cycle). PEEP can be beneficial if it recruits collapsed alveoli (lowers dynamic strain) and harmful if it overinflates them (increases dynamic strain). Driving pressure (ΔP) can be measured as plateau pressure minus PEEP. The plateau pressure depends on the respiratory system compliance (CRS). Studies demonstrate that higher driving pressures may worsen clinical outcome intraoperatively.^[19,20] It is also suggested that PEEP must be set to maximize respiratory system compliance to reduce the dynamic strain in all patients requiring mechanical ventilation during general anesthesia.^[21,22] However, a recent study has shown that the driving pressure may reflect changes in compliance only if the end-expiratory volume is less than the predicted functional residual capacity (FRC). If PEEP has overdistended the lung and the aerated volume exceeds FRC, monitoring driving pressure may not reflect changes in compliance. Thus, the authors' caution against the use of C_{RS} and ΔP as intraoperative monitoring tools during general anesthesia.^[23] The utility of monitoring driving pressure intraoperatively needs further studies.

In summary, with deeper understanding of physiology and availability of sophisticated devices, mechanical ventilation during general anesthesia has undergone a sea change from the simple automaticity of the anesthetist's hands to more precise ventilation with consequent improvement in outcome.

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